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Songjian Zhao^{a,b,1}, Wanmiao Chen^{a,c,1}, Wenjun Huang^a, Jiangkun Xie^a, Zan Qu^a, Naiqiang Yan^{a,*}

^a School of Environmental Science and Engineering, Shanghai Jiao Tong University, 800 Dong Chuan Road, Shanghai, 200240, PR China

ABSTRACT

^b School of Chemistry and Chemical Engineering, Shanghai Jiao Tong University, 800 Dong Chuan Road, Shanghai, 200240, PR China

^c Shanghai Institute of Pollution Control and Ecological Security, Shanghai 200092, China

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The mercury emission from coal-fired flue gas has drawn lots of attention worldwide. To achieve more efficient catalytic oxidation of Hg⁰ in both high and low temperature, the RuO₂ modified Ce-Zr solid solution catalysts were prepared and evaluated at various conditions. It was found the polyvinylpyrrolidone (PVP) promoted RuO₂/Ce_{0.6}Zr_{0.4}O₂ catalyst displayed higher significant catalytic activity for Hg⁰ oxidation. The mechanism of Hg⁰ oxidation over RuO₂/Ce_{0.6}Zr_{0.4}O₂(PVP) was studied through various techniques, and Hg⁰ oxidation approaches were found to consist of two steps: chemisorption process and regeneration process. The adsorbed Hg⁰ was first oxidized with surface chemisorbed oxygen species to form HgO, which could desorb from the surface of catalysts by itself in absence of HCl. Also, the HgO could reacts with Cl⁻ in catalyst or adsorbed HCl to form HgCl₂, which could desorb into gas phase more readily. O₂ is indispensable for the chemisorption process. And the doping RuO₂ might have a synergistic effect with supporter, which could facilitate chemisorption process. Furthermore, SeO₂ poisoning of catalyst was investigated for the first time and found the existence of SeO₂ could slightly inhibit Hg⁰ chemical adsorption process on the surface of the catalyst, while the regeneration process did not significantly affect.

1. Introduction

Mercury is a heavy metal pollutant with toxicity, bioaccumulation and persistence [1]. Superabundant anthropogenic emission of mercury into the atmosphere has attracted extensive attention worldwide and an international treaty (the Minamata Convention on Mercury) regarding mercury pollution was officially signed in 2013 [2,3]. Coal-fired power plants are primary anthropogenic mercury pollution sources in China and the United States due to their huge coal consumption. Mercury in coal-fired flue gas generally presents in three forms: elemental mercury (Hg⁰), gaseous oxidized mercury (Hg²⁺) and particulate-bound mercury (Hg^P), which mainly depends on the chlorine content of coal and combustion conditions [4]. Most of the oxidized and particulate-bound mercury can be readily captured with typical air pollution control devices (APCDs). However, Hg⁰ is the dominant mercury species that escapes into the atmosphere from coal-fired flue gas due to the highly volatile and insoluble. Therefore, the catalytic oxidation of Hg⁰ to Hg² with HCl from flue gas, is an economical way to obtain greater mercury removal efficiency with the existing APCDs [4-8], instead of additional

particular equipment for mercury. For example, the catalysts involved in selective catalytic reduction (SCR) of NO_x process were investigated as potential Hg⁰ conversion catalysts when sufficient HCl was present in flue gas [4,9]. However, the presence of ammonia (NH₂), employed as the SCR reductant, can significantly inhibit Hg⁰ oxidation over conventional SCR catalysts [9,10]. Therefore, the oxidation of Hg⁰ mainly occurs at the tail section of the SCR unit, which has lower NH₃ concentration.

In our previous study, a novel multi-functional catalyst (SCR-Plus) was proposed to be installed at the tail-end of SCR units [11], which would cooperate with SCR units to convert Hg⁰ and unreacted ammonia simultaneously. Moreover, the low temperature SCR catalysts have drawn lots of attention and are a tendency in future industrial application. To cooperate with low temperature SCR catalysts, new catalyst which could convert elemental mercury and ammonia significantly at low temperature should be developed.

Recently, ceria(Ce)-zirconia(Zr) solid solution with cubic fluorite phase (Ce:Zr > 1:1), has been employed in many studies as catalyst carrier and drawn much attention ascribable to its excellent oxygen

* Corresponding author.

E-mail address: nqyan@sjtu.edu.cn (N. Yan).

¹ These two authors contributed equally to this work.

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storage capacity and outstanding redox properties [12,13]. Moreover, Ce-Zr solid solution supported metal oxide catalysts have served for De-NOx and display excellent performance for NO reduction [14]. Therefore, Ce-Zr solid solutions could be a promising catalyst carrier for the multi-functional (SCR-Plus) catalysts. What's more, it has been proposed in many studies that the oxidation of Hg⁰ over catalysts with the presence of HCl might follow through Deacon reaction, in which HCl is converted to Cl₂ or Cl atom by oxygen [15-17]. And RuO₂ has been proven to be a very active component for Deacon reaction in many studies [18]. So RuO₂ is expected to be a potential catalyst component for Hg⁰ conversion with the presence of HCl. In our previous research, we had already found that RuO2 modified Ce0.6Zr0.4O2 displayed significant catalytic activity for selective oxidation of NH₃ [19], but the activity of the RuO₂ modified Ce_{0.6}Zr_{0.4}O₂ on mercury oxidation is still unclear. Many mechanisms of mercury removal such as Mars-Maessen mechanism, Eley-Rideal mechanism and Langmuir-Hinshelwood mechanism [4,20,21], have been proposed for mercury oxidation over different catalysts [17]. However, the mechanism of mercury removal over RuO₂ modified Ce_{0.6}Zr_{0.4}O₂ has scarcely been clarified. Especially, the role of Cl in the process of elemental mercury oxidation is barely involved and remains indistinct. Thus, the mechanism of mercury oxidation is the main focus in this study.

Since Ru is usually considered as a noble metal and is more expensive than most of the transition metals, the content of RuO_2 was set at very low level (0.2%). To maintain the catalytic performance of the catalyst while using lower Ru content, sol-gel method with polyvinylpyrrolidone(PVP) was employed to enhance the dispersion of RuO_2 on catalyst surface.

Selenium (Se) is one of trace elements in coal during combustion. The average concentration of selenium in U.S. coals is 2.8 ppm [22]. When coal is burnt, more than 97% of Se in coal will be volatilized at 800 °C and existed with the form of SeO₂. About 637 t Se and 236 t As were introduced into atmosphere from coal combustion in China in 2009 [23]. Many studies have reported that As would make the catalyst deactivation [24], and Se in coal gas might have negative effect and due to the similar amount to As. However, there were no reports about the effect of SeO₂ poisoning for Hg⁰ oxidation, so it was necessary to study the SeO₂ poisoning of catalysts.

In this study, elemental mercury removal efficiencies and adsorption behavior over various modified catalysts were evaluated. Also, possible catalytic mechanism of elemental mercury was studied, the role of RuO₂ and Cl in the oxidation was discussed especially. Moreover, the effect of SeO₂ poisoning of catalyst was investigated

2. Materials and methods

2.1. Preparation of catalysts

Please refer to the Supporting Information.

2.2. The loading method of SeO_2 poisoning

The catalyst nanoparticles were placed in the reactor with quartz wool firstly, and then some amount of SeO₂ were placed on the top of catalyst, which was purged by the flue gas with 4% O₂ and N₂ from top to bottom. And the furnace temperature raised slowly to 350 °C lasting for some time. The catalyst of loading was prepared and the sketch of SeO₂ loading shown in Supporting information (Fig. S1).

2.3. Catalytic activity measurement

The performance of the catalysts of Hg^0 adsorption and oxidation were tested in fixed-bed quartz reactor and the experiment system is shown in Supporting information (Fig. S2). The catalyst particles were placed in the reactor with quartz wool under atmospheric pressure, which was heated by a vertical electrical furnace. The feed gases were adjusted by mass flow controller and imported into the reactor with a total flow rate of 500 ml/min. The stable gas with elemental mercury from a permeation tube of Hg^0 , flowed through the blank tube and the reactor tube to provide mercury signals. The mercury concentration was monitored by MD254 (LabTech) and Tekran 3300 mercury analyzer.

During mercury adsorption, the flow with Hg^0 firstly passed through the blank tube to provide original Hg^0 signal. After Hg^0 concentration was stable, the gas was switched to reactor tube to run the adsorption. For each Hg^0 catalytic oxidation experiment with HCl, the mercury contained gas was firstly introduced to pass the catalysts to undergo adsorption. After adsorption saturation was reached, the Hg^0 concentration in the outlet was measured as $[Hg^0]_1$. Then, the HCl or other gases was introduced into the gas and the Hg^0 concentration in the outlet was measured as $[Hg^0]_2$ until reaction equilibrium. The Hg^0 oxidation efficiency (E_{oxi}) over the catalysts was quantified by the following equation:

$$E_{oxi}(\%) = \frac{[Hg^0]_1 - [Hg^0]_2}{[Hg^0]_1} \times 100\%$$

3. Results and discussion

3.1. Catalytic activity

The catalytic oxidation efficiencies over catalysts were tested and evaluated under various conditions as shown in Fig. 1 (preliminary experiments showed the Ce_{0.6}Zr_{0.4}O₂ supported catalysts displayed superior catalytic activity). The Hg⁰ oxidation efficiencies over Ce_{0.6}Zr_{0.4}O₂ are both lower than 10% at 350 °C and 150 °C. While, the mercury removal efficiency over RuO2/Ce0.6Zr0.4O2 increases to approximately 80% and 70% at high and low temperature, respectively, which indicates the doping of only 0.2% RuO₂ could significantly facilitate the Hg⁰ conversion. Meanwhile, the synthesis method could also have an effect on the catalytic activities. The Hg⁰ oxidation efficiency over $RuO_2/Ce_{0.6}Zr_{0.4}O_2(PVP)$ increases to about 91% and 88% at high and low temperature, respectively. We propose that PVP might promote Ru dispersion over carrier just similar in other studies and the catalytic activity is enhanced in consequence [25]. Moreover, the effects of SO₂ on Hg⁰ oxidation were tested and the results show that the Hg⁰ removal efficiency is slightly restrained over all three catalysts at both high and low temperature. In addition, the Hg⁰ oxidation efficiency of RuO₂/



Fig. 1. The oxidation efficiencies of elemental mercury over various catalysts at different conditions.

The compositions in the gas were 4% O_2 and N_2 . The Hg^0 concentration in the gas was approximately 110 (\pm 10) $\mu g/m^3$. The amount of catalysts were 60 mg and the space velocity (SV) was approximately $3.8\times10^5\,\,h^{-1}$.



Fig. 2. H₂-TPR curves of $Ce_{0.6}Zr_{0.4}O_2$, $RuO_2/Ce_{0.6}Zr_{0.4}O_2$, $RuO_2/Ce_{0.6}Zr_{0.4}O_2$, $RuO_2/Ce_{0.6}Zr_{0.4}O_2$, RuO_2/ZrO_2 .



 $Ce_{0.6}Zr_{0.4}O_2(PVP)$ was greater than 95% in the simulated coal-fired flue gas (NO, NH₃, SO₂, H₂O, O₂ and N₂ balance) for long experimental duration (Fig. S3) and the results displayed catalysts had excellent durability for the complex components in flue gas.

3.2. H₂-TPR

To investigate the redox behavior of the catalysts, the temperature program reduction (TPR) by hydrogen for the Ce_{0.6}Zr_{0.4}O₂ and RuO₂/ $Ce_{0.6}Zr_{0.4}O_2$ catalysts were tested. These results are shown in Fig. 2. In the Ce_{0.6}Zr_{0.4}O₂ catalyst, a board reduction peak centered at about 580 °C, which is attributed to the reduction of the Ce⁴⁺ in the Ce-Zr solid solution [26,27]. A very weak peak at 130 °C appeared on profile of 0.2%RuO₂/ZrO₂, and the peak is ascribed to the reduction of welldispersed RuO_x species [28]. Since the ZrO₂ is very difficult to be reduced by H₂ at low temperature, the reduction peak about at 480 °C in profile of 0.2%RuO₂/ZrO₂ might be attributed to the interaction of Ru oxide and ZrO₂ support [28]. A strong peak appeared at about 110 °C over RuO₂/Ce_{0.6}Zr_{0.4}O₂ and RuO₂/Ce_{0.6}Zr_{0.4}O₂(PVP), which was much different with the profiles of Ce_{0.6}Zr_{0.4}O₂ and RuO₂/ZrO₂. This peak could not be attributed to the reduction of RuO₂ alone because content of RuO₂ is only 0.2% and the consumption of H₂ is much more than that of RuO₂/ZrO₂ (Table S1). Meanwhile, the large reduction peak at 580 °C caused by Ce⁴⁺ disappeared from profile of RuO₂/Ce_{0.6}Zr_{0.4}O₂, the strong peak at low temperature (about 110 °C) could be explained by the interaction between RuO₂ and catalyst support, which suggested Ru-Ce complex oxide might exist in the RuO₂/Ce_{0.6}Zr_{0.4}O₂ catalyst and the oxidation capacity at low temperature was significantly improved. And this might explain the results that efficiencies of mercury oxidation were much higher with the presence of RuO₂.

3.3. Hg⁰ adsorption

As we know, catalytic reaction is generally associated with adsorption. Therefore, to clarify the mechanism of mercury oxidation over the RuO₂ modified catalysts, the adsorption of Hg⁰ over various conditions were investigated and the results are shown in Fig. 3. Firstly, the fresh RuO₂/Ce_{0.6}Zr_{0.4}O₂ was tested until equilibrium and the adsorption capacity for Hg⁰ was 1.36 mg/g (curve A). After that, the Hg⁰ was suspended and the catalyst was purged with O₂ and N₂ balance for 2 h. Afterwards, the adsorption experiment of Hg⁰ was carried again over the purged catalyst and the adsorption curve was obtained as curve B in Fig. 3. As shown in result, the adsorption time was shortened and the



Fig. 3. (a) The adsorption curves of elemental mercury over various catalysts at 350 °C (b) The order of the adsorption experiment in Fig. 3(a). The space velocity (SV) was approximately 3.0×10^5 h⁻¹. The total flow rate was set at 500 ml/min. The amount of catalysts were 60 mg. Temperature was 350 °C. Treating with HCl + N₂: Mercury suspend, catalyst was treated with 15 ppm HCl + N₂ for 90 min and then purged with N₂ for 30 min. Treating with HCl + O₂ + N₂: Mercury suspend, catalyst was treated with 15 ppm HCl + 4% O₂ + N₂ for 90 min and then purged with 4%O₂ + N₂ for 30 min.

capacity regenerated to 0.84 mg/g, which meant portion of adsorbed mercury could desorb from the catalyst surface during purging and some active adsorption sites on the surface were regenerated. Then, the catalyst was treated under 15 ppm HCl, 4% O2 and N2 balance for 90 min and 4% O2 and N2 balance for 30 min to remove physical absorbed HCl, respectively. After the treatment, the Hg⁰ adsorption over the catalyst was carried again and the adsorption curve was curve C. The results showed that the adsorption capacity of $RuO_2/Ce_{0.6}Zr_{0.4}O_2$ was recovered and even promoted to 2.16 mg/g by HCl. After that, the catalyst was treated with HCl again and the adsorption curve could be acquired as curve D, which showed that the adsorption capacity of RuO₂/Ce_{0.6}Zr_{0.4}O₂ for Hg⁰ was recovered and increased significantly to 3.92 mg/g, approximately 3 times compared with fresh catalyst. Since Cl in catalysts would have important effects on mercury removal (both adsorption and catalysis), the adsorption experiment was carried over fresh Cl-free RuO₂/Ce_{0.6}Zr_{0.4}O₂ and Ce_{0.6}Zr_{0.4}O₂ catalyst and the adsorption capacity was only 0.2 and 0.11 mg/g, which was much lower than normal $RuO_2/Ce_{0.6}Zr_{0.4}O_2$ which contains Cl and indicated that chlorine played a significant role in Hg⁰ adsorption (discuss later).

Deacon Reaction mechanism in which HCl was firstly oxidized with O_2 to form Cl atom, was proposed to explain catalytic oxidation of



Fig. 4. Mercury adsorption over catalysts monitored with Terkan mercury analyzer. The space velocity (SV) was approximately 9.1×10^5 h⁻¹. The amount of catalysts was 25 mg. The temperature was 350 °C. (a) RuO₂/Ce_{0.6}Zr_{0.4}O₂, 4%O₂ and N₂ (b) RuO₂/Ce_{0.6}Zr_{0.4}O₂, N₂ (c) Cl-free RuO₂/Ce_{0.6}Zr_{0.4}O₂, 4%O₂ and N₂.

mercury in many studies [15–17]. Also, to evaluate the role of O₂ and interaction between HCl and O₂, another adsorption experiment was carried over the fresh RuO₂/Ce_{0.6}Zr_{0.4}O₂ catalyst. After the treating under 15 ppm HCl and N₂ without O₂, the adsorption capacity was also regenerated (curve F and G) and the adsorption curves were similar with results under HCl, 4% O₂ and N₂, which indicates that O₂ is not necessary for the regeneration process with HCl. Since HCl could have effects without O₂, which implies that Deacon reaction mechanism may not be appropriate explanation for mercury oxidation in this research. These results indicate that the elemental mercury oxidation over the RuO₂/Ce_{0.6}Zr_{0.4}O₂ catalyst consist of two separable process, the Hg⁰ adsorption process and the regeneration process with HCl.

To further investigate the adsorption of mercury over RuO_2 modified catalysts, the Tekran mercury analyzer which could directly monitor Hg^0 and Hg^T simultaneously, was employed to detect the adsorption process and the results are shown in Fig. 4. Some amount of oxidized mercury (Hg^{2+}) was generated when the Hg^0 passed through the RuO_2 modified catalyst with RuCl_3 as precursor (Fig. 4(a)) and it demonstrated that elemental mercury could be oxidized without gaseous HCl. The result in Fig. 4(b) was acquired by carrying the Hg^0 adsorption without O_2 over RuO_2 modified catalyst with RuCl_3 as precursor. Only little amount of oxidized mercury was detected during the initial stage of adsorption, which could be oxidized by surface chemisorbed oxygen in the catalysts (discuss later). The results prove that adsorption and oxidation of mercury are negligible without O₂. Similar experiment was carried out over the Cl-free RuO₂/Ce_{0.6}Zr_{0.4}O₂ (C₁₄H₂₇O₁₈Ru₃ as precursor) and the results are shown in Fig. 4(c). Elemental mercury could still be oxidized over the Cl-free RuO₂/Ce_{0.6}Zr_{0.4}O₂ catalyst with O₂, but the oxidized mercury (Hg²⁺) concentration was much less compared with that of catalyst with RuCl₃ as precursor and elemental mercury slipping from the catalyst was much higher. It could be inferred from the results that O₂ is indispensable for mercury adsorption, and elemental mercury is firstly adsorbed and oxidized with O₂ on the catalyst and then the oxidized mercury (Hg²⁺) desorbed from the surface of catalyst. The Cl⁻ in catalyst is not necessary for the mercury oxidation, but it could promote oxidation of Hg⁰.

3.4. Mechanism of catalytic oxidation of Hg⁰

To further determine the mechanism of elemental mercury oxidation, the catalytic oxidation of Hg^0 with HCl was also carried out and monitored by the Tekran mercury analyzer. As the result in Fig. S4 shows, when some amount of mercury (about 110 ng/L) passed through the RuO₂/Ce_{0.6}Zr_{0.4}O₂(PVP), approximately 68 ng/L oxidized mercury (Hg²⁺) could be detected in the gas. And when the HCl was added into the gas, the total mercury (Hg^T) concentration increased to about 136 ng/L rapidly. Afterthat, the Hg^T decreased rapidly to about 77 ng/



Fig. 5. Mechanism of mercury oxidation over RuO₂/Ce_{0.6}Zr_{0.4}O₂.

L, and then increased slowly. When HCl was introduced into the gas, portion of the HgO on the surface of the catalyst could react with HCl to form $HgCl_2$ and desorbed from the surface, which led the momentary increase of Hg^{T} . Since desorption of the oxidized mercury was accelerated and the active adsorption sites on the surface were regenerated by HCl, the adsorption (both physical and chemical) of elemental mercury was enhanced. In this way, the concentration of the elemental mercury in gas decreased to very low level as shown in Fig. S4 and the Hg^{T} also reduced to some degree. When the reaction equilibrium was researched, the Hg^{T} recovered to original concentration (about 110 ng/L) and the mercury was balanced during the catalytic reaction.

Above all, the catalytic oxidation of elemental mercury on the surface with the presence of HCl contains two separate steps: chemisorption process and the regeneration process (as shown in Fig. 5). Firstly, the Hg⁰ in gas is adsorbed to the surface of the catalysts and adsorbed ${\rm Hg}^0$ then is oxidized to ${\rm Hg}^{2+}$ by the active oxygen species from metallic oxides catalysts (Reactions (1) and (2)). The O 1s XPS spectrum on catalyst after Hg⁰ adsorption without O₂ and fresh catalyst are shown in Fig. S5. The peak at 529.5 eV might be ascribed to lattice oxygen, and the peak at 531.4 eV could be attributed to surface chemisorbed oxygen [29]. Besides, the peak at 529.5 eV was nucleophilic states, and 531.4 eV peak denoted electrophilic states for the O 1s which was beneficial for oxidation reaction [30]. And it was found in the XPS results that the ratio of surface chemisorbed oxygen on catalyst decreased from 29.1% to 20.4% after Hg^0 adsorption without O_2 , which displayed that the adsorbed Hg⁰ was oxidized by the surface chemisorbed oxygen species.

The adsorption of elemental mercury on $Ce_{0.6}Zr_{0.4}O_2$ without HCl is shown in Fig. S6, and the conversion of Hg⁰ is much lower than that of RuO₂/Ce_{0.6}Zr_{0.4}O₂(PVP) in absence of HCl. This result displayed that the doping of RuO₂ could facilitate the chemisorption process because the oxidation ability of the catalyst is enhanced as shown in H₂-TPR results. Also, some studies proposed that O₂ was more easily be dissociated with the presence of RuO₂, which might accelerate the replenishing of surface chemisorption process could occur without chlorine (neither gasous HCl nor Cl⁻ on surface), but the O₂ in gas is essential for this step. When no chlorine exists in the catalysts or gas, the oxidized mercury could also desorb from the surface of the catalysts (Reaction (3)). This reaction pathway could explain the results in Fig. S4 that elemental mercury could still be oxidized by the catalysts in absence of HCl.

$$\mathrm{Hg}^{0}(g) \to \mathrm{Hg}^{0}(ads) \tag{1}$$

$$Hg^{0}(ads) + O \to HgO(ads)$$
⁽²⁾

$$HgO(ads) \rightarrow HgO(g)$$
 (3)

$$HCl(g) \rightarrow HCl(ads)$$
 (4)

$$HgO(ads) + 2HCl(ads) \rightarrow HgCl_2(ads) + H_2O$$
 (5)

$$\operatorname{HgCl}_2(ads) \to \operatorname{HgCl}_2(g)$$
 (6)

$$Hg + 2HCl + O_2 \rightarrow HgCl_2 + H_2O$$
(7)

When HCl exists in the gas, the oxidized mercury could react with the adsorbed HCl and HgCl₂ is generated (Reactions (5) and (6)). Since the HgCl₂ could more readily desorb from the surface of the catalysts, the regeneration of active sites on the catalysts are accelerated by the HCl. It had already been proven in research that the presence of HCl could facilitate the release of oxidized mercury into gas phase [32]. The Cl⁻ in catalyst could also expedite the release of oxidized mercury into the gas phase and regeneration of active adsorption sites, and this could explain the results in Fig. 3 that the adsorption capacity of Hg⁰ over RuO₂/Ce_{0.6}Zr_{0.4}O₂ was improved significantly by HCl treatment. What's more, the effects of Cl could explain the results that the oxidation efficiencies of elemental mercury were much higher in presence of HCl.

3.5. The effect of SeO_2 on Hg^0 catalytic oxidation

In order to study the loading of SeO₂, X-ray fluorescence (XRF) analysis was performed for different catalysts loaded with SeO₂ and the results are shown in Table S2. All the results in the table are based on 30 mg of the catalyst, using different SeO₂ loading amount. The Se content in the table indicates the result by the XRF test, and the Se adhesion ratio indicates the ratio of actual test Se content and theoretically Se content assumed all SeO₂ attached the catalyst. It can be seen that with the increase of the amount of SeO₂ loading amount, the adhesion ratio of Se does not significantly increase or decrease, which are fluctuated within a relatively small range of 15%–20%, indicated that the load ratio of SeO₂ is basically kept at a relatively stable level during the experimental process and can be used to research the Hg⁰ catalytic oxidation.

Fig. S7 shows the effect of SeO₂ on Hg^0 catalytic oxidation. The fresh catalyst had a high Hg^0 catalytic oxidation efficiency, with 99% at 5 ppm HCl. However, the oxidation efficiency reduced after loading SeO₂ on RuO₂/Ce_{0.6}Zr_{0.4}O₂(PVP). With the amount increase of SeO₂, the Hg^0 oxidation efficiency declined slowly until loading 5 mg SeO₂. And then when the loading amount of SeO₂ reached 9 mg, the catalytic performance of RuO₂/Ce_{0.6}Zr_{0.4}O₂ had no obviously variation with the increase of SeO₂. It indicated that SeO₂ was bad for the Hg^0 catalytic oxidation, and might inhibit the oxidation reaction process.

The effect of SO₂ on RuO₂/Ce_{0.6}Zr_{0.4}O₂(PVP) poisoning by SeO₂ was also studied. It can be seen that SO₂ had an inhibitory effect for Hg⁰ catalytic oxidation, which might be possibly that SO₂ is adsorbed at the active site, inhibiting the reaction of Hg⁰ and chlorine species. While the effect reduced when the loading amount of SeO₂ was above 5 mg, which might because the poisoning mechanism of SeO₂ and SO₂ was similar due to the same family of Se and S elements. And when the amount of SeO₂ was high, the active site SO₂ attached was little, so the influence of SO₂ is relatively small.

The pathway of elemental mercury oxidation over the $RuO_2/Ce_{0.6}Zr_{0.4}O_2$ catalyst consists of two steps above: chemisorption process and regeneration process. So the effect of SeO₂ on the two steps was studied, respectively.

3.5.1. The effect of SeO_2 for Hg^0 chemisorption process

Fig. S8 shows the adsorption curves of fresh and SeO₂ poisoned



Fig. 6. The Ce XPS spectrum of fresh and SeO $_2$ poisoned RuO $_2$ /Ce $_{0.6}$ Zr $_{0.4}$ O $_2$ (PVP) catalysts.

 $RuO_2/Ce_{0.6}Zr_{0.4}O_2(PVP)$ catalysts. As can be seen from Fig. S8, fresh catalyst had a certain Hg^0 adsorption ability, but not high. The concentration of Hg^0 presented a trend increasing earlier and then

decreasing, and reached about 70% of initial mercury concentration, indicated the oxidation efficiency was about 30%. When ${\rm Hg}^0$ was passed through SeO₂ poisoned catalyst, the Hg⁰ concentration

presented the similar variation tendency compared with that of fresh catalyst. After reaching reaction equilibrium, Hg^0 concentration accounted for about 77% of initial mercury concentration, manifested the Hg^0 oxidation efficiency was about 23%, lower than fresh catalyst. It suggested that SeO₂ would affect the chemisorption mechanism.

3.5.2. The effect of SeO_2 for regeneration process

The adsorption curves of HCl treated fresh and SeO₂ poisoned were studied, shown in Fig. S9. Consistent with results of Fig. 3, the Hg⁰ adsorption ability of fresh RuO₂/Ce_{0.6}Zr_{0.4}O₂ enhanced obviously due to the HCl treatment, and Hg⁰ removal efficiency reach above 90% within 250 min. SeO₂ poisoned catalyst had the similar Hg⁰ adsorption ability, indicated that SeO₂ had little effect on the process of HCl adsorption and combination with HgO into HgCl₂.

Through the above two adsorption experiment, as can know SeO_2 poisoning can slightly inhibit Hg^0 chemical adsorption process on the surface of the catalyst, the reaction of (1)–(3) was affected negatively. While the regeneration process did not significantly affect, manifested that the reaction of (4) and (5) can be proceeded normally for SeO₂ poisoned catalyst.

3.5.3. The analysis of poisoned mechanism

To investigate the effect of SeO₂ poisoning for redox ability of catalyst, H₂-TPR experiment of fresh and poisoned catalyst was operated, shown in Fig. S10. The reduction peak of Ce-Zr and 0.2%RuO₂/Ce_{0.6}Zr_{0.4}O₂ were mentioned in Fig. S10. And the reduction peaks of SeO₂ poisoned catalyst presented different peak position and shape compared with fresh catalyst. Firstly, the strong peak located at about 110 °C disappeared, which was assigned to the interaction between RuO₂ and catalyst support. And there was a board peak started from 200 °C, and the peak value was located at about 470 °C with shoulder peak at about 300 °C. It indicated that the loading SeO₂ changed obviously the redox ability of catalyst. The strong peak at 470 °C might be due to the interaction of Se and Ce oxide, while the shoulder peak can be attributed to the composite oxide of Ru and Se. The results of TPR indicated that SeO₂ poisoning reduced the oxidation ability of catalyst at low temperature, so that the Hg⁰ chemisorption was worse.

The XPS spectrum of fresh and SeO₂ poisoned RuO₂/ Ce_{0.6}Zr_{0.4}O₂(PVP) catalysts were analyzed to study the chemical valence variation of element due to the SeO₂ poisoning, shown in Fig. 6. The XPS spectrum of Zr 3d (Fig. 6(a)) can be deconvoluted into two peaks for Zr 3d5/2 and Zr 3d3/2, located at around 182.5 eV and 185 eV respectively, which was attributed to the zirconium in the Zr⁴⁺ state [33]. After loading SeO₂, the proportion of characteristic peak at 184.7 eV increased from approximately 42% to 61%, indicated that the existing form of Zr was affected by SeO₂.

The CeO₂ spectrum was composed of two multiplets (v and u), where V and U correspond to the spin-orbit split 3d 5/2 and 3d 3/2 core holes, respectively. The peaks referred to as u0, u2, u3, v0, v2, v3 are contributed by CeO₂ and assigned to Ce IV (3d¹⁰4f⁺), while the peak of u1 and v1 are assigned to Ce III (3d¹⁰4f⁺) [34]. The proportion of Ce³⁺ / (Ce³⁺ + Ce⁴⁺) could calculate by the area of these peaks. The proportion of Ce³⁺ of RuO₂/Ce_{0.6}Zr_{0.4}O₂ were approximately 30%, which was reduced to 20% after loading. And the existence of Ce³⁺ can induce the charge imbalance cavitation and unsaturated bonds, which can make the chemical adsorption of oxygen on the surface of catalyst increase and promote the catalytic activity.

It can be seen from Fig. 6 the proportion of chemical adsorption of oxygen decreased from approximately 61% to 39% when loading SeO₂. The analysis above has shown that Hg^0 chemisorption process primarily depended on the surface adsorption oxygen. And the results of XPS spectrum show that the existence of SeO₂ could suppress the Hg^0 chemical adsorption activity of catalyst, consistent with the results in Fig. S8.

4. Conclusions

In conclusion, the PVP promoted 0.2%RuO₂ modified Ce_{0.6}Zr_{0.4}O₂ catalyst displayed excellent catalytic oxidation activity for elemental mercury with various conditions at both high and low temperature. The pathway of elemental mercury oxidation over the RuO₂/Ce_{0.6}Zr_{0.4}O₂ catalyst was found to consist of two steps: chemisorption process and regeneration process. That is the adsorbed Hg⁰ is first oxidized with surface chemisorbed oxygen species to form HgO. The HgO could desorb from the surface of catalysts in absence of HCl. And also, the HgO could reacts with Cl⁻ from surface of catalyst or adsorbed HCl to form HgCl₂, which is more readily to desorb into the gaseous phase, O₂, which could replenish the consumption of surface chemisorbed oxygen. is indispensable for the chemisorption process. And the doping of RuO₂ could have synergistic effect with supporter and facilitate chemisorption process, which led the results that RuO₂ modified catalysts displayed significant performance for elemental mercury removal. Besides, loading SeO₂ can slightly inhibit Hg⁰ chemical adsorption process on the surface of the catalyst, while the regeneration process did not significantly affect.

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Appendix A. Supplementary data

Supplementary material related to this article can be found, in the online version, at doi:https://doi.org/10.1016/j.apcata.2018.07.022.

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